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## DETERMINING THE TENSILE PROPERTIES OF STRAIN HARDENING CEMENTITIOUS COMPOSITES BY FOUR POINT BENDING TEST

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### ABSTRACT:

As emerging advanced construction materials, Strain Hardening Cementitious Composites (SHCCs) have seen increasing field applications recently, yet existing test methods for quality control of tensile properties are relatively complicated and sometime difficult to implement. This paper presents a new simple inverse method for quality control of tensile strain capacity and tensile strength by conducting four point bending test (FPBT). First the beam deflection capacity and modulus of rupture (MOR) can be obtained from FPBT. The beam deflection capacity can then be linearly transformed to tensile strain capacity via a master curve constructed from parametric studies of beam flexural model [1]. Knowing the MOR and predicted tensile strain capacity, the effective tensile strength can be derived based on a new set of master curve. This proposed method has been experimentally verified with independent uniaxial tensile test results with reasonable agreement. In addition, this proposed method is also compared with Japan Concrete Institute method with comparable accuracy, yet with much simpler experiment setup and data interpretation procedure. Therefore, it is expected that this proposed method can greatly simplify the quality control of SHCCs both in execution and interpretation phases, contributing to the wider acceptance of this type of new material in field applications.

**Keywords:** Tensile properties, Strain hardening cementitious composites (SHCCs), Four point bending test (FPBT), Quality control, inverse method

### 1. INTRODUCTION

In the past decade, great strides have been made in developing strain hardening cementitious composite (SHCC), characterized by its unique macroscopic pseudo strain hardening behavior after first cracking under uniaxial tension. SHCCs, also referred to as high performance fiber reinforced cementitious composites (HPRCCs [2]), develop multiple cracks under tensile load in contrast to single crack and tension softening behavior of concrete and conventional fiber reinforced concrete. Multiple cracking provides a means of energy dissipation at the material level and prevent catastrophic fracture at the structural level, thus contributing to structural safety. Meanwhile, material tensile strain hardening (ductility) has been gradually recognized as having a close connection with structural durability [3] by suppressing localized cracks with large width. Many deterioration and premature failure of infrastructure can be traced back to the brittle nature of concrete. Therefore, SHCCs are considered a promising material solution to the global infrastructure deterioration problem and its tensile behavior is of major interest.

While most characterization of the tensile behavior of SHCCs was carried out using uniaxial tensile test (UTT) in academia, this method is generally considered to be complicated, time-consuming and require advanced equipment and delicate experimental skills. Therefore, it is not suitable for onsite quality control purpose [4,5,6].

As a simpler alternative to the UTT, four point bending test (FPBT) was proposed by Stang and Li [4] for quality control on construction sites, provided that an appropriate interpretation (inverse) procedure for the test result is available. This type of test is much simpler and puts much less demand on equipment and experimental skills compared to UTT, and extensive experience has been accumulated in the user community. The ultimate goal of this test is to use the moment-curvature or moment-deflection curves so determined to invert for the uniaxial tensile properties. It should be noted, however, that the bending test is not meant to determine whether the material has tensile strain-hardening behavior or tension-softening behavior, but rather to constrain the material tensile properties, e.g. the tensile strain capacity or tensile strength, as part of the quality control process in the field, for a material mix designed to exhibit strain-hardening. The inverse

procedure is the key to the success of FPBT to achieve the intended purpose, and it must be sufficiently accurate yet simple enough for field practice.

Inverse analyses for FPBT have recently been attempted by researchers at Technical University of Denmark (DTU), Japan Concrete Institute (JCI) and University of Michigan (UM) [1,5,6] with certain success. Both the JCI and UM methods are based on a simplified elastic-plastic tensile model and can generally predict tensile properties from the FPBT results via a sectional analysis similar to that developed by Maalej and Li [7]. On the other hand, hinge model, including both tensile strain hardening and tension softening effect, was employed in the DTU inverse method along with least square method to invert for tensile material properties from their bending response. The model can predict experimental load – deflection curve fairly well and tensile properties derived based on this method agree well with that from FEM analysis, yet no direct comparison with UTT results has been made so far.

The UM method may be more appealing to the user community compared with the JCI method due to improvement in terms of experimental execution (no need for LVDTs) and data interpretation procedure (simple linear transformation instead of solving complicated cubic equations) yet with similar accuracy [1]. Nevertheless, unlike the JCI method, the existing UM method can only predict tensile strain capacity, which sometimes can limit its usefulness for quality control of SHCCs. In large scale field application of SHCCs, tensile strength has also been commonly monitored besides tensile strain capacity due to its importance in the structural application [8, 9]. Therefore, the UM method has to be further developed to be able to predict the tensile strength in order to make it an efficient and comprehensive quality control method for SHCCs materials.

In this paper, the UM method will be extended to include prediction for both tensile strain capacity and tensile strength. In the following sections, parametric study to obtain the master curves for inverse analysis will be described first. Thereafter, the experimental program consisting of both FPBT and complementary UTT will be briefly reviewed. The results from FPBT will then be converted to tensile strength and validated with independent UTT test results. Finally, the extended UM method will be compared with JCI inverse method, followed by overall conclusions.

## 2. OVERALL INVERSE PROCEDURE

The overall inverse procedure is revealed in Figure 1. As a first step, MOR and corresponding deflection capacity,  $\delta_u$ , can be obtained from FPBT. Based on authors' previous work [1], tensile strain capacity,  $\epsilon_u$ , can be derived from deflection capacity based on a linear master curve (shown in dash-line box). By

conducting parametric studies based on a flexural behavior model of SHCCs, a new master curve can be constructed in terms of MOR/effective tensile strength,  $\sigma_{te}$ , with respect to tensile strain capacity. With predicted tensile strain capacity and this new master curve from parametric study, effective tensile strength of SHCCs can be derived.

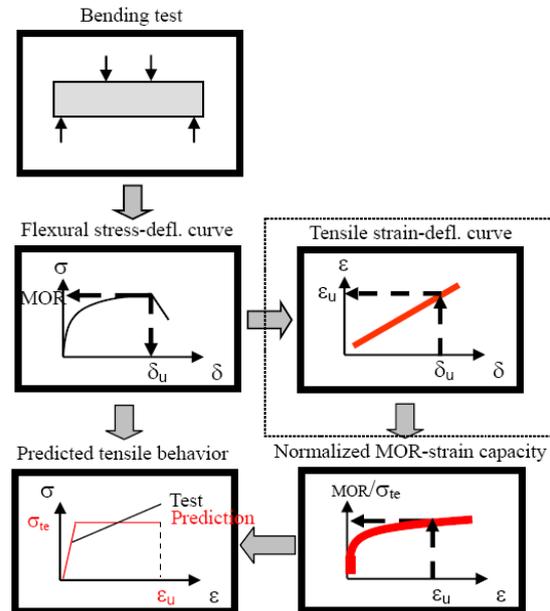


Figure 1 Sketch of inverse procedure of extended UM method (Tensile strain-deflection curve shown in dash-line box is the master curve developed in Qian and Li [1])

## 3. PARAMETRIC STUDY AND MASTER CURVES

### 3.1 Flexural Behavior Model

The flexural behavior model used in this investigation is based on the work of Maalej and Li [7]. Compared with other models, the major distinction of this model is that the contribution of tensile strain hardening property of SHCCs was included. The actual SHCC considered in the model is Polyethylene ECC (PE-ECC) material. To simplify the analysis, the stress-strain behavior of the ECC was assumed as bilinear curves in both tension and compression. Based on a linear strain profile and equilibrium of forces and moment in the beam section, the relation between flexural stress and tensile strain at the extreme tension fiber (Simplified as critical tensile strain hereafter) can be determined as a function of basic material properties. Due to the linear relation between critical tensile strain and deflection, the flexural stress and deflection relation can then be established. Overall, the model predicts experimentally measured flexural response quite well. For more detail, the readers are referred to Maalej and Li [7].

As an illustration of capability of the model, Maalej and Li [7] found out that the ratio of modulus of rupture over first crack strength ( $MOR/\sigma_{tc}$ ) increases as a function of tensile strain capacity  $\epsilon_{tu}$ . The rate of increase is initially high, and as  $\epsilon_{tu}$  becomes larger than 0.01, the rate of increase becomes very small. The model indicates that the initial high slope of the ( $MOR/\sigma_{tc}$ )- $\epsilon_{tu}$  curve is associated with a significant increase in the size of the microcracking zone as the ultimate tensile strain increases. When  $\epsilon_{tu}$  becomes large, the size of the microcracking zone reaches about 90% of the beam depth and does not significantly change as  $\epsilon_{tu}$  continues to increase. This suggests that the MOR of the polyethylene ECC would not significantly change as a result of an increase in the ultimate tensile strain of the material beyond about 1%. On the other hand, the MOR of the polyethylene ECC can be increased by increasing the tensile first cracking strength and/or the ultimate tensile strength.

While the above ( $MOR/\sigma_{tc}$ )- $\epsilon_{tu}$  relation is derived based on only one particular SHCC (PE-ECC) by varying its tensile strain capacity and resulting in different MOR, it does suggest that such a relation, if holds true for a wide range of material tensile and compressive properties, will provide a basis for inverse analysis of the tensile strength from MOR. This will be investigated in the following parametric studies and a master curve to correlate the ratio of MOR to tensile strength with  $\epsilon_{tu}$  will be established. To simplify the inverse process and minimize the unknowns, however, it is advisable to assume that the hardening modulus of SHCCs in tension is zero, i.e, the first cracking strength is equal to the ultimate tensile strength.

Table 1: Range of material parameters used in parametric studies to construct the normalized MOR - tensile strain capacity relation

Tensile properties		Comp. properties	
Effective tensile strength (MPa)	Tensile strain capacity (%)	Comp. strength (MPa)	Comp. strain capacity (%)
2.5~16.0	0~5	31~200	0.5~1

### 3.2 Construction of Master Curves

A parametric study was conducted to investigate the influence of material uniaxial tensile and compressive properties (parametric values) on the flexural response of SHCCs based on the aforementioned flexural model. To simplify the inverse process, the first cracking strength is assumed to be equal to the ultimate tensile strength and will be labeled as the effective tensile strength hereafter. The correlation between the normalized MOR (by effective tensile strength) and the tensile strain capacity was established. All tensile and compressive properties were varied within a wide range

of parametric values (Table 1), covering the normal range of test results of SHCC specimens at UM and JCI [6]. It is expected that the master curves based on this wide range of parametric study can be directly utilized for quality control purpose in field.

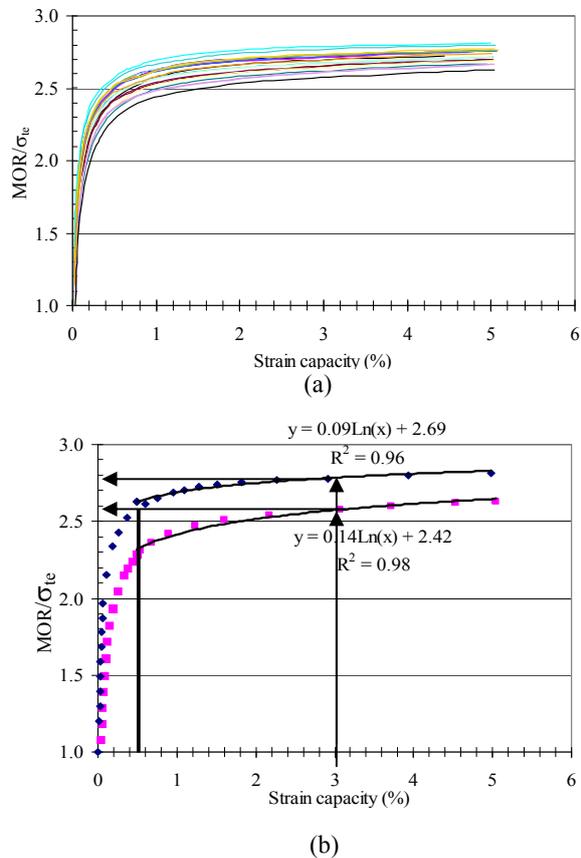


Figure 2: Relation of  $MOR/\sigma_{te}$  with tensile strain capacity for (a) all cases with UM and JCI data (smoothed lines from actual data points) and (b) two extreme cases with up and lower boundaries (It is not recommended to use this master curve to invert for  $\sigma_{te}$  when the strain capacity is less than 0.5%; y and x means  $MOR/\sigma_{te}$  and strain capacity, respectively)

The overall results from the parametric study indeed show a fairly good correlation between the normalized MOR and the tensile strain capacity, as revealed in Figure 2 (a). Totally 20 cases were investigated in the parametric study, with the range of material parameters shown in Table 1. All curves lie in a relatively narrow band regardless of actual material properties, which suggests that the normalized MOR is most sensitive to the tensile strain capacity, at least when the tensile strain is less than 1%. Normalized MOR shows a plateau when the tensile strain exceeds 1%, which suggests that it is almost independent of tensile strain capacity. For ease of quality control on site, master curve was constructed with two lines (up and lower limits) to cover all parametric case studies, as shown in Figure 2(b).

It is well known that for an elastic-perfectly plastic material like metal, the normalized MOR ( $MOR/\sigma_{tc}$ ) is equal to 3, in which case  $\sigma_{tc}$  is the yield strength. For an elastic-ideally brittle material like glass, the normalized MOR is equal to 1. Figure 2 shows that for SHCC material, this same ratio is bracketed between 1 and 3 depending on the tensile strain capacity. Note that for SHCC, the compression block does not follow the elastic-perfectly plastic behavior.

Additionally, another master curve correlating the normalized MOR with the tensile strain capacity was constructed by parametric study based on the JCI standard beam specimen in order to compare the proposed UM method with the JCI method. The range of material parametric values is the same as the aforementioned parametric study in Table 1. The dimension of the specimens used in this parametric study is 100x100x400mm, with a span length of 300mm (JCI-S-003-2007 [10]).

As expected, this set of master curve coincides with the one shown in Figure 2, especially in terms of upper bound and lower bound. This can be understood from the fact that the normalized MOR is a dimensionless number, which should be independent of geometry (beam height) of specimen. It should be noted however that the master curve relating deflection capacity to tensile strain capacity is dependent on the geometry of the specimen [1]. When two master curves are expected to be used together for quality control, a standard size of specimen should be specified.

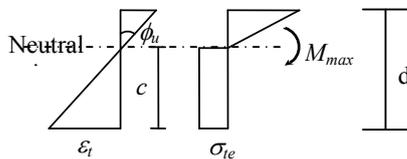


Figure 3 Assumption of strain and stress distribution along beam section

### 3.3 Discussion on the Unique Behavior of Master Curves

The master curve reveals a plateau with a relatively narrow band width when tensile strain capacity exceeds 1%. In the following, discussions will be presented to provide some understanding of this unique phenomenon.

As shown in Figure 3, a simple model of sectional analysis similar to Kanakubo [6] was adopted to facilitate the easy derivation of the relation of normalized MOR with tensile strain capacity. When tensile strain capacity is sufficiently large, e.g. 1%, the result from this simple model should yield comparable result to that from more complicated model such as Maalaj and Li model [7], which was used in the parametric study to obtain the master curve.

From both force equilibrium and moment equilibrium, following two equations can be derived:

$$\frac{E \cdot b \cdot \phi_u}{2} \cdot (d - c)^2 = \sigma_{te} \cdot b \cdot c \quad (1)$$

$$M_{max} = \frac{E \cdot b \cdot \phi_u}{3} \cdot (d - c)^3 + \frac{\sigma_{te} \cdot b}{2} \cdot c^2 \quad (2)$$

where  $E$  is the static modulus of elasticity ( $N/mm^2$ );  $b$  is the width of specimen (mm);  $\phi_u$  is the curvature capacity ( $1/mm$ );  $d$  is the depth of the specimen (mm);  $c$  is the distance from extreme tension fiber to the neutral axis (mm);  $\sigma_{te}$  is the predicted effective tensile strength (MPa);  $M_{max}$  is the maximum moment ( $N \cdot mm$ ).

The above equations can be simplified to obtain the expression for effective tensile strength and MOR as follows:

$$\sigma_{te} = \frac{E \cdot \phi_u}{2c} \cdot (d - c)^2 \quad (3)$$

$$MOR = \frac{6M_{max}}{bd^2} = 2E \cdot d \cdot \phi_u \cdot (1 - \frac{c}{d})^3 + 3\sigma_{te} \cdot (\frac{c}{d})^2 \quad (4)$$

The ratio of MOR over effective tensile strength can then be derived as a function of  $c_0$  or  $c/d$ :

$$\frac{MOR}{\sigma_{te}} = 4(\frac{c}{d}) - (\frac{c}{d})^2 = 4c_0 - c_0^2 \quad (5)$$

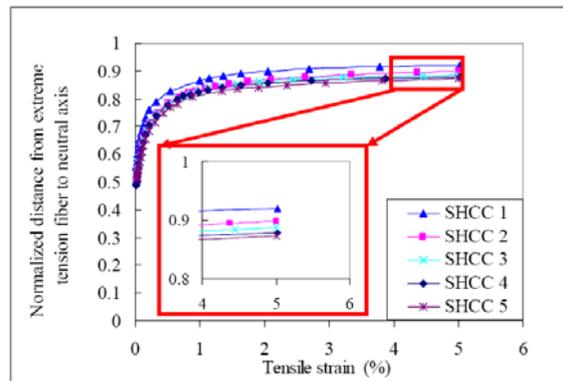


Figure 4 Normalized distance from extreme tension fiber to neutral axis (distance normalized by the beam height) – tensile strain capacity ( $c_0 - \epsilon_{tu}$ ) relation for SHCCs

According to Qian and Li [1],  $c_0$  shows a plateau value of around 0.9 once  $\epsilon_{tu}$  exceeds 1%, as can be seen in Figure 4. The corresponding normalized MOR is about 2.8, which agrees reasonably well with the master curve shown in Figure 2. Furthermore, it is observed that these  $c_0$  values near plateau are very close for cases with drastically different material properties. This explains the narrow band width of the master curve. It should be noted, however, that the above equation (5)

should not be used for cases when  $\epsilon_{tu}$  is well below 1%, e.g. when  $c_0$  equals to 0.5 (corresponding  $\epsilon_{tu}$  of 0%) due to the great simplification of stress distribution mentioned previously.

### 3.4 Use of Master Curves

Based on the master curves obtained from parametric study, the MOR from simple beam bending test can be easily converted to effective tensile strength. Assuming a tensile strain capacity of 3% already being inverted from deflection capacity, the corresponding value of MOR/ $\sigma_{te}$  can then be found from the master curve, including both upper and lower bound values (2.8 and 2.58 respectively). Assuming an MOR of 12 MPa obtained from experimental bending test, the effective tensile strength will then be 4.29 MPa and 4.65 MPa. In order to be on the conservative side for quality control purpose, the upper boundary of the master curve may be used, which will give a lower value of effective tensile strength. The calculation of standard deviation of the effective tensile strength can then use the same upper bound value given the standard deviation of MOR is known. The master curve is not recommended for use for tensile strain capacity less than 0.5% due to the steep slope of the master curve at the initial stage.

A set of equations has been developed by curve fitting to simplify the conversion procedure, as shown below, where Equations (6) and (7) can be used to calculate the effective tensile strength, including both lower limit  $\sigma_{te}^1$  and upper limit  $\sigma_{te}^2$ , respectively.

$$\sigma_{te}^1 = \frac{MOR}{0.09Ln(\epsilon_{tu}) + 2.69} \quad (6)$$

$$\sigma_{te}^2 = \frac{MOR}{0.14Ln(\epsilon_{tu}) + 2.42} \quad (7)$$

where  $\epsilon_{tu}$  is the tensile strain capacity (%), Ln is natural logarithm and  $R^2$  is 0.96 and 0.98 for Equations (6) and (7), respectively.

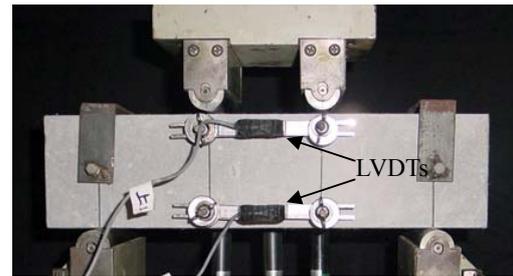
As mentioned previously, the master curve can only be applied for use for tensile strain capacity larger than 0.5% due to the steep slope of the master curve at the initial stage. Similarly, the above equations can only be utilized for derivation of effective tensile strength when the tensile strain capacity exceeds 0.5%.

### 4. EXPERIMENTAL SETUP AND RESULTS

The mix proportion of SHCC materials investigated in this study is shown in Table 2, including M 1, 2 and 3. These SHCC materials feature high amount of fly ash in the mix proportion, with fly ash to cement ratios of 1.2, 2.0, and 2.8, respectively. The experimental results from these mixtures will be used for comparison between the UM method and the JCI method.



(a)



(b)

Figure 5: Comparison of test setup for the (a) UM method and (b) JCI method

Table 2: Mix proportion for different SHCCs

	C	S	FA	W/B	SP	Fiber
M 1	1	0.8	1.2	0.27	0.013	0.02
M 2	1	1.1	2	0.26	0.014	0.02
M 3	1	1.4	2.8	0.26	0.016	0.02

(C: cement; S: sand; FA: fly ash; W/B: water binder ratio; SP: superplasticizer)

A Hobart mixer was used in this investigation, with a full capacity of 12 liters. All beam, uniaxial tensile and compressive specimens were cast from the same batch. The beam and uniaxial tensile specimens were cast horizontally and compressive cylinder specimens were cast vertically. At least 3 specimens were prepared for each test. After demolding, all specimens were cured in a sealed container with about 99% humidity under room temperature for 28 days before testing. Four point bending test was conducted with a MTS 810 machine. The test setup is shown in Figure 5 (a) in comparison with the JCI method (Figure 5 (b)). Uniaxial tensile test (UTT) with “fix-fix” end condition was also carried out to directly verify the derived effective tensile strength from four point bending test. For more details on the experiments, the readers are referred to Qian and Li [1].

The material tensile, compressive properties and bending properties for different SHCCs can be found in Tables 3. The deflection capacity and corresponding MOR obtained from these curves can then be used to invert the tensile strain capacity and effective tensile strength.

Table 3: Tensile properties from 2D UTT test and compressive strength for M 1, 2 and 3

	First cracking strength (MPa)	Ultimate tensile strength (MPa)	Tensile strain capacity (%)	Comp. strength (MPa)
M 1	4.6±0.3	5.3±0.6	2.1±1.1	54.6±6.5
M 2	3.9±0.5	4.6±0.2	3.5±0.3	46.0±3.8
M 3	4.0±0.2	4.9±0.1	3.7±0.4	37.5±1.7

Table 4: Comparison between effective tensile strength predicted from FPBT and first cracking strength/tensile strength from 2D UTT test

	First cracking strength	Ultimate tensile strength	Effective tensile strength (lower limit)	Effective tensile strength (upper limit)
M 1	4.6±0.3	5.3±0.6	4.3±0.1 (-7%)	4.7±0.1 (2%)
M 2	3.9±0.5	4.6±0.2	3.6±0.2 (-7%)	4.0±0.2 (2%)
M 3	4.0±0.2	4.9±0.1	3.9±0.2 (-2%)	4.2±0.2 (5%)

(Note: The number in parenthesis is the difference between the predictions and first cracking strength from uniaxial tensile test; all units are in MPa)

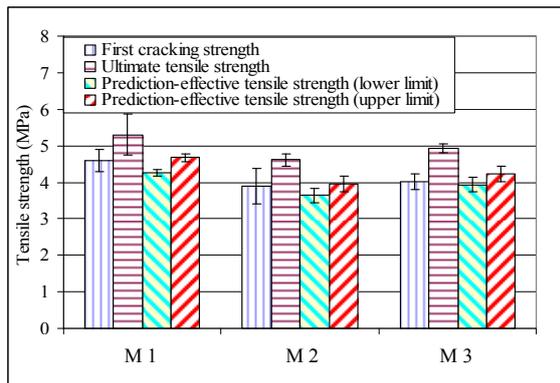


Figure 6: Comparison of UTT results and predicted effective tensile strength based on extended UM method for M1, 2 and 3

### 5. VALIDATION AND VERIFICATION OF THE PROPOSED METHOD

To validate the proposed inverse method, the MOR obtained from FPBT is converted to effective tensile strength using Equations (1) and (2) and then compared with first cracking strength and/or tensile strength obtained directly from uniaxial tensile test for M 1-M3. As revealed in Table 4 and Figure 6, the effective tensile strength (both lower and upper limits) derived from FPBT seems to match the first cracking strength with reasonable accuracy, with less than 10% difference. This agreement demonstrates the validity of the proposed inverse method. Furthermore, the lower limit prediction may be used in order to be conservative for quality control purpose.

To further verify the proposed UM method, comparison between the UM method and the JCI method was conducted based on JCI round robin test data (Kanakubo [6]). As mentioned previously, the bending test results from the JCI round robin test are presented in the form of moment-curvature relation. Within the JCI method, the effective tensile strength is obtained by solving the following equations (JCI-S-003-2007 [10]):

$$f_{t,b} = \frac{E \cdot \phi_u \cdot D \cdot x_{nl}^2}{2(1 - x_{nl})} \quad (8)$$

$$x_{nl} = -1 + 2 \cos \frac{\theta}{3} \quad (9)$$

$$\theta = \arccos(-1 + 6m^*) \quad (10)$$

$$m^* = \frac{M_{max}}{E \cdot \phi_u \cdot B \cdot D^3} \quad (11)$$

where  $f_{t,b}$  is the predicted effective tensile strength (MPa);  $E$  is the static modulus of elasticity (N/mm<sup>2</sup>);  $\phi_u$  is the curvature capacity (1/mm), which can be calculated from two LVDTs measurements (Figure 5 (b));  $D$  is depth of the test specimen (=100 mm);  $x_{nl}$  is the ratio of the distance from compressive edge (extreme compression fiber) to neutral axis over depth of test specimen, which needs to be solved from Equations (9-11);  $M_{max}$  is maximum moment (N·mm);  $B$  is the width of test specimen (100 mm). For more details, readers are referred to the Appendix to JCI-S-003-2007 [10].

As shown in Figure 7, predictions based on both the UM method and the JCI method reveal comparable results with those from uniaxial tensile tests of 3D specimens. This is consistent with the expectation that the fiber orientation in the flexural beam geometry is probably closer to 3-D. Furthermore, the tensile test results from 2D specimens generally shows higher tensile strength compared with that from 3D specimens as expected. In particular, the tensile strength of SF-SHCC in 2D specimens may be artificially boosted by its long steel fiber (15mm) mixed within very small cross-section (13mmx30mm). Tensile strength of PE-SHCC is lower in 2D compared with that in 3D may be due to different casting direction and/or done by different groups with different fresh rheology (Kanakubo [6]). The overall consistency between the UM method and the JCI method and verification by independent JCI round robin test data further demonstrate the validity of the proposed UM method.

The advantage of the UM method over the JCI method lies in its simplicity, both in the experimental and data

interpretation phases. In the experimental phase, the UM method requires only machine displacement to be measured. This is not the case for the JCI method, where complicated setup such as LVDTs is needed to measure curvature, as revealed in Figure 5 (a) and (b). In the data interpretation phase, the UM method only needs a simple master curve or equation to convert MOR directly into effective tensile strength, while the JCI method requires relatively complicated procedures to obtain effective tensile strength. Considering the large amount of specimens needed to be tested during construction, the UM method seems to be more suitable for quality control purpose due to its simplicity, efficiency and reasonable accuracy.

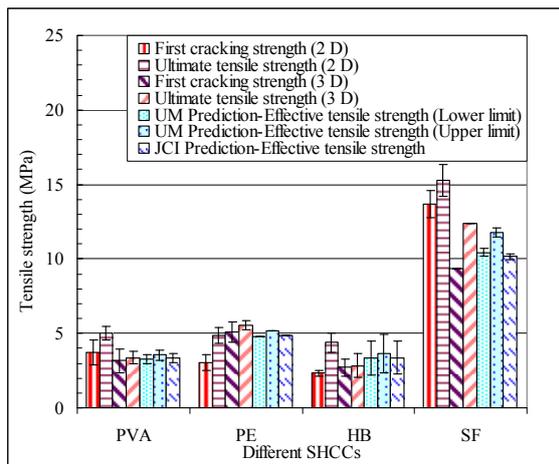


Figure 7 Comparison of UTT results and predicted effective tensile strength based on extended UM and JCI method for different SHCCs

## 6. CONCLUSIONS

To facilitate the quality control of the strain hardening cementitious composites on site, a simplified inverse method is proposed to convert the MOR from simple beam bending test to effective tensile strength through simple transformation. The simple transformation (in the form of master curves) is derived from parametric study with a wide range of parametric values of material tensile and compressive properties based on a theoretical model. This proposed method has been experimentally validated with uniaxial tensile test results. In addition, this proposed method compares favorably with the JCI method in accuracy, but without the associated complexity.

The following specific conclusions can be drawn from this study:

(1) A simple inverse method has been successfully developed to derive effective tensile strength of SHCC from MOR of beam bending test by using a master curve. This method is expected to greatly ease the on-site quality control for SHCC in terms of much simpler experiment setup requirement (compared with both UTT and the JCI inverse method) and data

interpretation procedure (compared with the JCI method), yet with reasonable accuracy (generally within 11% if the lower limit prediction is used for conservativeness);

(2) The master curve features relatively simple transformation with a narrow band width. The master curve decouples the dependence of effective tensile strength on the curvature capacity in contrast with the JCI method where effective tensile strength is dependent on both curvature capacity and moment capacity. Therefore, this method allows relatively simple equations (Equation (6) and (7)) to be used for easy data interpretation;

(3) A plateau value of around 2.7-2.8 is observed for master curve when the strain capacity exceeds 1%. It has been shown that this plateau value is closely related to the fact that the neutral axis of the SHCCs under bending rapidly approaches the extreme compression fiber and quickly stabilizes (the plateau distance from extreme tension fiber to neutral axis is about 90% of the beam depth); Once the strain capacity exceeds 1%, the effective tensile strength is almost fully dependent on MOR only.

(4) The master curve itself is not dependent on the geometry of the specimen, in contrast to the previous master curve relating the tensile strain capacity with deflection capacity (Qian and Li [1]). When these two sets of master curves are used together to determine both the tensile strain capacity and the effective tensile strength, however, a standard geometry of specimen must be specified.

It should be noted that the following assumptions are made when the proposed UM method is used: (a) The tested material is truly a strain hardening type; (b) The major target for quality control for this material is tensile strength and tensile ductility; and (c) For this method to be most effective, a standardized beam with fixed geometric dimensions should be agreed upon by the user community.

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